

Research Article

Peristaltic Transport of a Jeffrey Fluid with Variable Viscosity through a Porous Medium in an Asymmetric Channel

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The peristaltic flow of a Jeffrey fluid with variable viscosity through a porous medium in an asymmetric channel is investigated. The channel asymmetric is produced by choosing the peristaltic wave train on the wall of different amplitude and phase. The governing nonlinear partial differential equations for the Jeffrey fluid model are derived in Cartesian coordinates system. Analytic solutions for stream function, velocity, pressure gradient, and pressure rise are first developed by regular perturbation method, and then the role of pertinent parameters is illustrated graphically.

1. Introduction

Peristalsis is a mechanism to pump the fluid by means of moving contraction on the tubes or channel walls. This process has quite useful applications in many biological systems and industry. It occurs in swallowing food through the esophagus, chyme motion in the gastrointestinal tract, the vasomotion of small blood vessels such as venules, capillaries, and arterioles, urine transport from kidney to bladder, sanitary fluid transport of corrosive fluids, a toxic liquid transport in the nuclear industry, and so forth. In view of such physiological and industrial applications, the peristaltic flows has been studied with great interest by the various researchers for viscous and non-Newtonian fluids [1–9].

In most of the studies which deal with the peristaltic flows, the fluid viscosity is assumed to be constant. This assumption is not valid everywhere. In general the coefficients of viscosity for real fluids are functions of space coordinate, temperature, and pressure. For many liquids such as water, oils, and blood, the variation of viscosity due to space coordinate and temperature change is more dominant than other effects. Therefore, it is highly desirable

to include the effect of variable viscosity instead of considering the viscosity of the fluid to be constant. Some important studies related to the variable viscosity are cited in [10–13].

A porous medium is the matter which contains a number of small holes distributed throughout the matter. Flows through a porous medium occur in filtration of fluids. Several investigations have been published by using generalized Darcy's law where the convective acceleration and viscous stress are taken into account [14–17].

Considering the importance of non-Newtonian fluid in peristalsis and keeping in mind the sensitivity of liquid viscosity, an attempt is made to study the peristaltic transport of Jeffrey having variable viscosity through a porous medium in a two-dimensional asymmetric channel under the assumption of long wave length and the low Reynolds number approximation. A regular perturbation method is used to solve the problem, and the solutions are expanded in a power series of viscosity parameter α . The obtained expressions are utilized to discuss the influences of various emerging parameters.

2. Mathematical Formulation

We consider an incompressible Jeffrey fluid in an asymmetric channel of width $d_1 + d_2$. A sinusoidal wave propagating with constant speed c on the channel walls induces the flow. The wall surfaces are chosen of the following forms:

$$\begin{aligned} H_1(X, t) &= a_1 + b_1 \cos \left[\frac{2\pi}{\lambda} (X - ct) \right], & \text{upper wall,} \\ H_2(X, t) &= -a_2 - b_2 \cos \left[\frac{2\pi}{\lambda} (X - ct) + \phi \right], & \text{lower wall,} \end{aligned} \quad (2.1)$$

where b_1, b_2 are amplitude of the upper and lower waves, λ is the wave length, ϕ is the phase difference which varies in the range $0 \leq \phi \leq \pi$. Furthermore, a_1, a_2, b_1, b_2 , and ϕ should satisfy the following condition

$$b_1^2 + b_2^2 + 2b_1b_2 \cos \phi \leq (a_1 + a_2)^2. \quad (2.2)$$

We assume that the flow becomes steady in the wave frame (x, y) moving with velocity c away from the fixed (laboratory) frame (X, Y) . The transformation between these two frames is given by

$$x = X - ct, \quad y = Y, \quad u = U - c, \quad v = V, \quad p(x) = P(X, t), \quad (2.3)$$

where u and v are the velocity components in the wave frame (x, y) , p and P are pressure in wave and fixed frame of reference, respectively. The governing equations in the wave frame of reference are the Brinkman extended Darcy equations given by

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \quad (2.4)$$

$$\rho \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -\frac{\partial p}{\partial x} + \frac{1}{\varepsilon} \frac{\partial \tau_{xx}}{\partial x} + \frac{1}{\varepsilon} \frac{\partial \tau_{xy}}{\partial y} - \frac{\mu(y)}{k} (u + 1), \quad (2.5)$$

$$\rho \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) = -\frac{\partial p}{\partial y} + \frac{\partial \tau_{yx}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} - \frac{\mu(y)}{k} v, \quad (2.6)$$

where

$$\begin{aligned} \tau_{xx} &= \frac{2\mu(y)}{(1 + \lambda_1)} \left[1 + \lambda_2 \left(u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right) \right] \frac{\partial u}{\partial x}, \\ \tau_{xy} &= \frac{\mu(y)}{(1 + \lambda_1)} \left[1 + \lambda_2 \left(u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right) \right] \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right), \\ \tau_{yy} &= \frac{2\mu(y)}{(1 + \lambda_1)} \left[1 + \lambda_2 \left(u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right) \right] \frac{\partial v}{\partial y}, \end{aligned} \quad (2.7)$$

where λ_1 is the ratio of relaxation to retardation times, λ_2 is the retardation time, ρ is the density, k is the permeability of the porous medium, and ε is the porosity of the porous medium.

Introducing the following nondimensional quantities:

$$\begin{aligned} \bar{x} &= \frac{x}{\lambda}, \quad \bar{y} = \frac{y}{a_1}, \quad \bar{u} = \frac{u}{c}, \quad \bar{v} = \frac{v}{c\delta}, \quad h_1 = \frac{H_1}{a_1}, \quad h_2 = \frac{H_2}{a_1}, \quad \bar{\tau} = \frac{a_1 \tau}{\mu_0 c} \\ \bar{t} &= \frac{ct}{\lambda}, \quad \text{Da} = \frac{k}{a_1^2}, \quad \delta = \frac{a}{\lambda}, \quad \bar{p} = \frac{pa_1^2}{\mu_0 c \lambda}, \quad a = \frac{b_1}{a_1}, \quad b = \frac{b_2}{a_1}, \quad d = \frac{a_2}{a_1}. \end{aligned} \quad (2.8)$$

With the help of (2.8), (2.4) to (2.6) after dropping the bars take the form

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \quad (2.9)$$

$$\text{Re} \delta \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = -\frac{\partial p}{\partial x} + \frac{\delta}{\varepsilon} \frac{\partial \tau_{xx}}{\partial x} + \frac{1}{\varepsilon} \frac{\partial \tau_{xy}}{\partial y} - \frac{\mu(y)}{\text{Da}} (u + 1), \quad (2.10)$$

$$\text{Re} \delta^3 \left(u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) = -\frac{\partial p}{\partial y} + \frac{\delta^2}{\varepsilon} \frac{\partial \tau_{xy}}{\partial x} + \frac{\delta}{\varepsilon} \frac{\partial \tau_{yy}}{\partial y} - \frac{\delta^2 \mu(y)}{\text{Da}} v, \quad (2.11)$$

where Darcy's number is

$$\begin{aligned} \text{Da} &= \frac{k}{a_1^2}, \\ \tau_{xx} &= \frac{2\delta\mu(y)}{(1+\lambda_1)} \left[1 + \frac{\lambda_2\delta c}{a_1} \left(u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right) \right] \frac{\partial u}{\partial x}, \\ \tau_{xy} &= \frac{\mu(y)}{(1+\lambda_1)} \left[1 + \frac{\lambda_2\delta c}{a_1} \left(u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right) \right] \left(\frac{\partial u}{\partial y} + \delta^2 \frac{\partial v}{\partial x} \right), \\ \tau_{yy} &= \frac{2\mu(y)}{(1+\lambda_1)} \left[1 + \frac{\lambda_2\delta c}{a_1} \left(u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right) \right] \frac{\partial v}{\partial y}. \end{aligned} \quad (2.12)$$

Using the longwave length and small Reynolds number approximation, (2.10) and (2.11) take the form

$$\frac{\partial p}{\partial x} = \frac{1}{\varepsilon} \frac{\partial}{\partial y} \left[\frac{\mu(y)}{(1+\lambda_1)} \frac{\partial u}{\partial y} \right] - \frac{\mu(y)}{\text{Da}} (u+1), \quad (2.13)$$

$$\frac{\partial p}{\partial y} = 0. \quad (2.14)$$

The corresponding boundary conditions are

$$u = -1, \quad \text{at } y = h_1, \quad (2.15a)$$

$$u = -1, \quad \text{at } y = h_2, \quad (2.15b)$$

where

$$h_1 = 1 + a \cos 2\pi x, \quad h_2 = -d - b \cos(2\pi x + \phi). \quad (2.15c)$$

Equation (2.14) indicate that p is independent of y . Therefore, (2.10) can be written as

$$\frac{dp}{dx} = \frac{1}{\varepsilon} \frac{\partial}{\partial y} \left[\frac{\mu(y)}{(1+\lambda_1)} \frac{\partial u}{\partial y} \right] - \frac{\mu(y)}{\text{Da}} (u+1), \quad (2.16)$$

where $\mu(y)$ is the viscosity variation on peristaltic flow. For the present analysis, we assume viscosity variation in the dimensionless form [10]:

$$u(y) = e^{-\alpha y}, \quad u(y) = 1 - \alpha y + \frac{\alpha y^2}{2}, \quad \text{for } \alpha \ll 1. \quad (2.17)$$

The volume flow rate in the wave frame is given by

$$q = \int_{h_2}^{h_1} u \, dy. \quad (2.18)$$

The instantaneous flux $Q(x, t)$ in the laboratory frame is defined as

$$Q(x, t) = \int_{h_1}^{h_2} (u + 1) \, dy = q + h_1 - h_2. \quad (2.19)$$

The average flux over one period ($T = \lambda/c$) is given by

$$\bar{Q} = \frac{1}{T} \int_0^T Q \, dt = \frac{1}{T} \int_0^T (q + h_1 - h_2) \, dt = q + 1 + d. \quad (2.20)$$

3. Perturbation Solution

Equation (2.16) is a nonlinear differential equation so that it is not possible to obtain a closed form solution; so we seek perturbation solution. We expand u , p and q as

$$\begin{aligned} u &= u_0 + \alpha u_1 + \alpha^2 u_2 + o(\alpha^3), \\ p &= p_0 + \alpha p_1 + \alpha^2 p_2 + o(\alpha^3), \\ q &= q_0 + \alpha q_1 + \alpha^2 q_2 + o(\alpha^3). \end{aligned} \quad (3.1)$$

Substituting these equations into (2.15a), (2.15b), (2.15c), and (2.16), we have the following system of equations.

3.1. Zeroth-Order Equations α^0

$$\frac{\partial^2 u_0}{\partial y^2} - N^2 u_0 = \varepsilon(1 + \lambda_1) \frac{dp_0}{dx} + N^2, \quad (3.2)$$

where

$$\begin{aligned} N &= \frac{\varepsilon(1 + \lambda_1)}{\text{Da}}, \\ u_0 &= -1, \quad \text{at } y = h_1, h_2. \end{aligned} \quad (3.3)$$

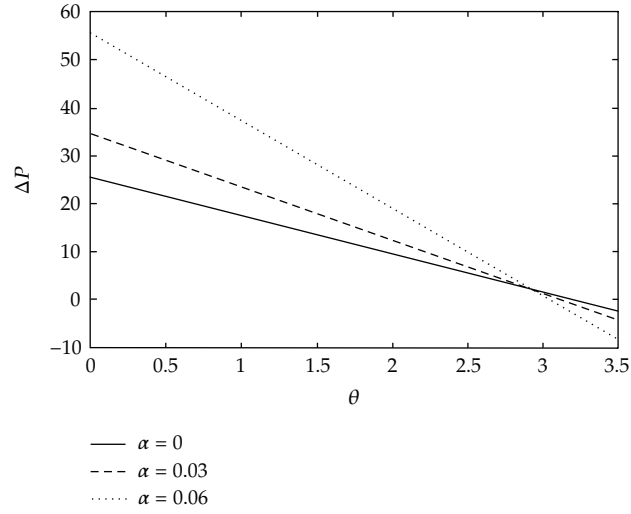


Figure 1: The pressure rise versus flow rate when $a = 0.2, b = 0.6, d = 0.8, \varepsilon = 0.3, \lambda_1 = 0.8, Da = 0.6,$ and $\phi = \pi/4$.

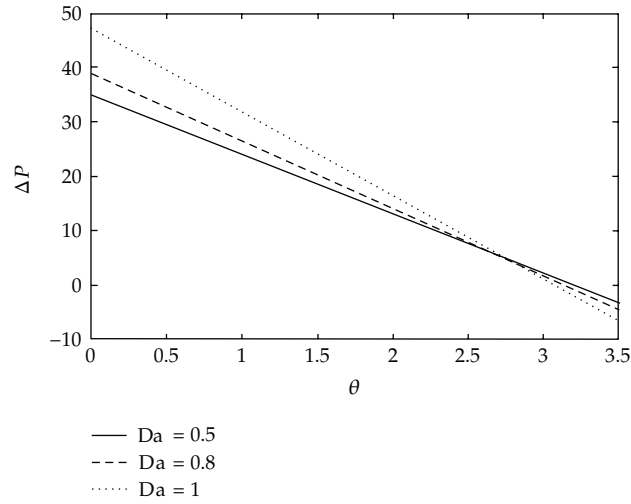


Figure 2: The pressure rise versus flow rate when $\alpha = 0.01, a = 0.2, b = 0.6, d = 0.8, \varepsilon = 0.3, \lambda_1 = 0.4,$ and $\phi = \pi/4$.

3.2. First-Order Equations α

$$\frac{\partial^2 u_1}{\partial y^2} - N^2 u_1 = \varepsilon(1 + \lambda_1) \frac{dp_1}{dx} + \varepsilon y(1 + \lambda_1) \frac{dp_0}{dx} + \frac{\partial u_0}{\partial y}, \quad (3.4)$$

$$u_1 = 0, \quad \text{at } y = h_1, h_2. \quad (3.5)$$

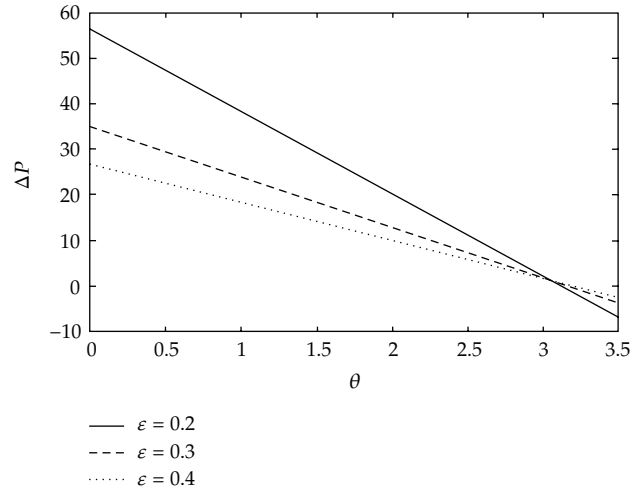


Figure 3: The pressure rise versus flow rate when $\alpha = 0.01$, $a = 0.2$, $b = 0.6$, $d = 0.8$, $\lambda_1 = 0.4$, $Da = 0.5$, and $\phi = \pi/4$.

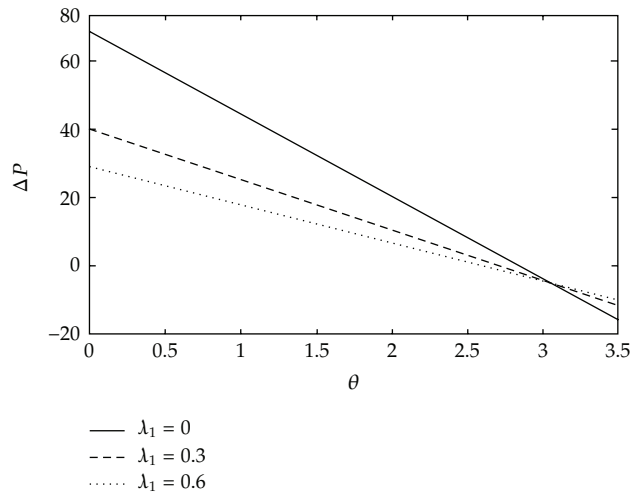


Figure 4: The pressure rise versus flow rate when $\alpha = 0.01$, $a = 0.2$, $b = 0.6$, $d = 0.8$, $\varepsilon = 0.3$, $Da = 0.8$, and $\phi = \pi/4$.

3.3. Second-Order Equations α^2

$$\frac{\partial^2 u_2}{\partial y^2} - N^2 u_2 = \varepsilon(1 + \lambda_1) \frac{dp_2}{dx} + \varepsilon(1 + \lambda_1) y \frac{dp_1}{dx} + \frac{y^2}{2} \varepsilon(1 + \lambda_1) \frac{dp_0}{dx} + \frac{\partial u_1}{\partial y}, \quad (3.6)$$

$$u_2 = 0 \quad \text{at } y = h_1, h_2. \quad (3.7)$$

3.4. Zeroth-Order Solution

Solving (3.2) and (3.3), we get

$$u_0 = \frac{\varepsilon(1 + \lambda_1)}{N^2} \frac{dp_0}{dx} [C_1 \cosh Ny + C_2 \sinh Ny - 1] - 1, \quad (3.8)$$

where

$$C_1 = \frac{(\sinh Nh_1 - \sinh Nh_2)}{\sinh N(h_1 - h_2)}, \quad C_2 = \frac{(\cosh Nh_2 - \cosh Nh_1)}{\sinh N(h_1 - h_2)}, \quad (3.9)$$

and the volume flow rate q_0 is given by

$$q_0 = \int_{h_2}^{h_1} u_0 dy. \quad (3.10)$$

From (3.8), we have

$$\frac{dp_0}{dx} = (q_0 + h_1 - h_2)A, \quad (3.11)$$

where

$$A = \frac{N^3 \sinh N(h_1 - h_2)}{\varepsilon(1 + \lambda_1)[2 \cosh N(h_1 - h_2) - 2 - (h_1 - h_2)N \sinh N(h_1 - h_2)]}. \quad (3.12)$$

The dimensionless pressure rise at this order is

$$\Delta P_0 = \int_0^1 \frac{dp_0}{dx} dx. \quad (3.13)$$

3.5. First-Order Solution

Substituting zeroth order solution (3.8) into (3.4) and then solving the resulting system along with the corresponding boundary conditions, we arrive at

$$\begin{aligned} u_1 = & \frac{\varepsilon(1 + \lambda_1)}{N^2} \frac{dp_1}{dx} [C_1 \cosh Ny + C_2 \sinh Ny - 1] \\ & + \frac{\varepsilon(1 + \lambda_1)}{2N^2} \frac{dp_0}{dx} \left[-2y + C_1 y \cosh Ny + C_2 y \sinh Ny \right. \\ & \quad \times \frac{\sinh Ny (h_1 \cosh Nh_2 - h_2 \cosh Nh_1)}{\sinh N(h_1 - h_2)} \\ & \quad \left. + \frac{\cosh Ny (h_2 \sinh Nh_1 - h_1 \sinh Nh_2)}{\sinh N(h_1 - h_2)} \right], \end{aligned} \quad (3.14)$$

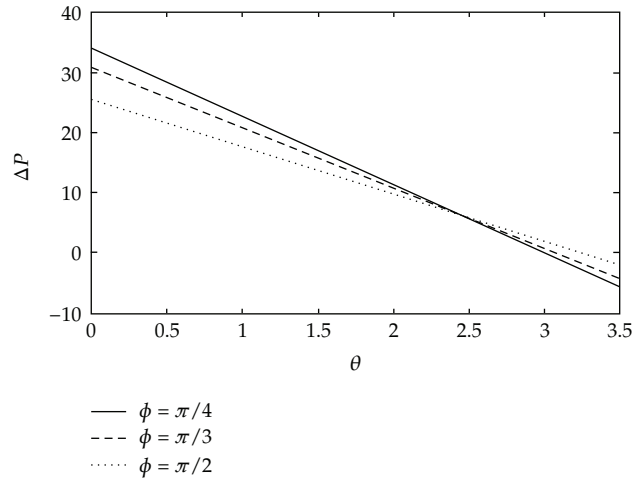


Figure 5: The pressure rise versus flow rate when $\alpha = 0.01$, $a = 0.4$, $b = 0.6$, $d = 0.8$, $\varepsilon = 0.4$, $\lambda_1 = 0.5$, and $Da = 0.5$.

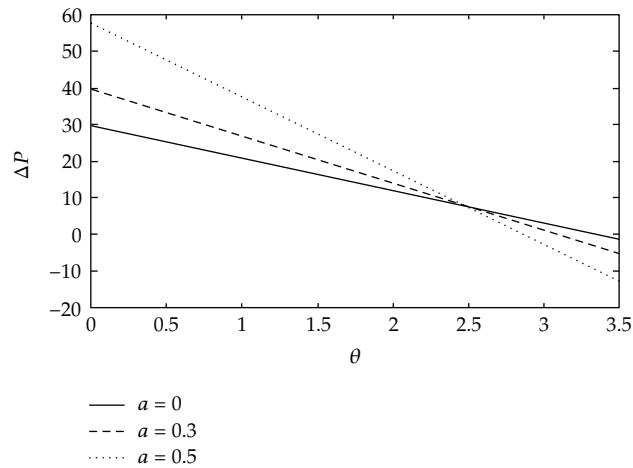


Figure 6: The pressure rise versus flow rate when $\alpha = 0.01$, $b = 0.6$, $d = 0.8$, $\varepsilon = 0.3$, $\lambda_1 = 0.4$, $Da = 0.5$, and $\phi = \pi/4$.

and the volume flow rate q_1 is given by

$$q_1 = \int_{h_2}^{h_1} u_1 dy. \tag{3.15}$$

From (3.14), we get

$$\frac{dp_1}{dx} = Aq_1 + \frac{A\varepsilon(1 + \lambda_1)}{2N^3} \frac{dp_0}{dx} \left[N^2 (h_1^2 - h_2^2) + \frac{(h_1 + h_2)(1 - \cosh N(h_1 - h_2))}{\sinh N(h_1 - h_2)} \right]. \tag{3.16}$$

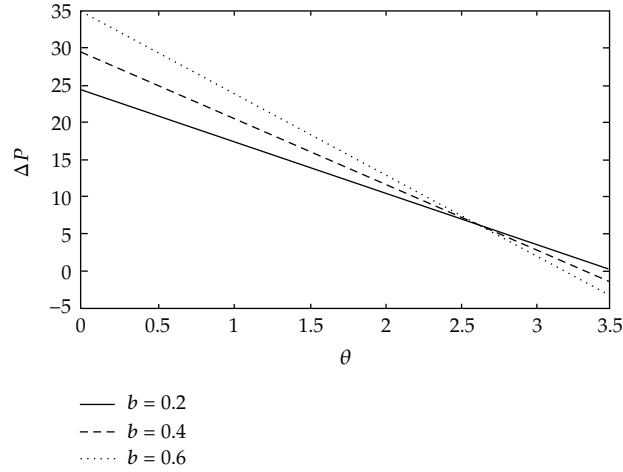


Figure 7: The pressure rise versus flow rate when $\alpha = 0.01$, $a = 0.2$, $d = 0.8$, $\varepsilon = 0.3$, $\lambda_1 = 0.4$, $Da = 0.5$, and $\phi = \pi/4$.

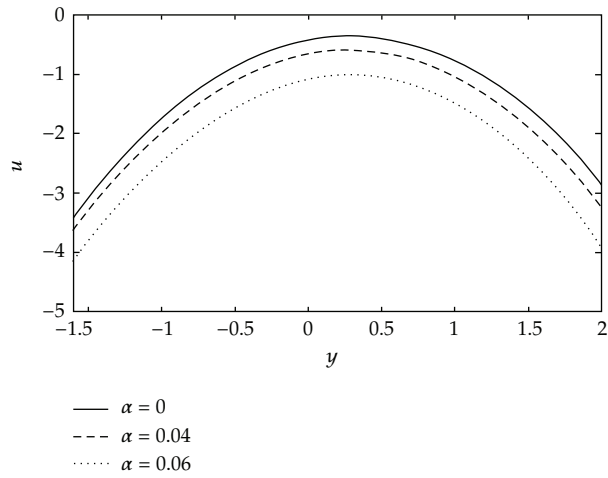


Figure 8: Axial velocity versus y at $a = 0.2$, $b = 0.6$, $d = 0.8$, $\varepsilon = 0.2$, $\lambda_1 = 1$, $Da = 1$, $x = \pi/6$, $q = -1$, and $\phi = \pi/2$.

The dimensionless pressure rise at this order is

$$\Delta P_1 = \int_0^1 \frac{dp_1}{dx} dx. \tag{3.17}$$

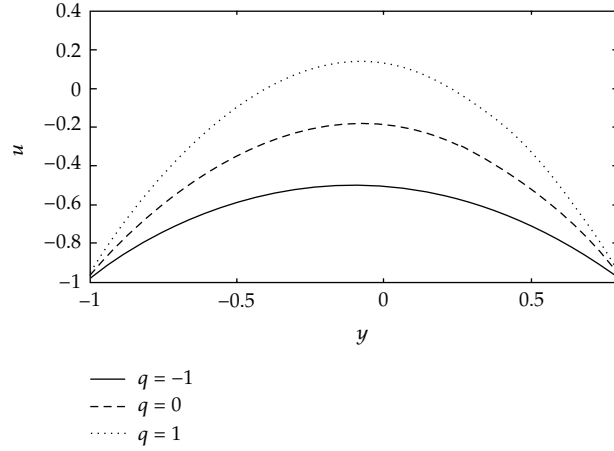


Figure 9: Axial velocity versus y at $\alpha = 0.05$, $a = 0.2$, $b = 0.6$, $d = 0.8$, $\varepsilon = 0.2$, $\lambda_1 = 1$, $Da = 1$, $x = 0$, and $\phi = \pi/2$.

3.6. Second-Order Solution

Solving (3.6) by using (3.8) and (3.14) and the boundary condition (3.5), we obtain

$$\begin{aligned}
 u_2 = & \frac{\varepsilon(1 + \lambda_1)}{N^2} \frac{dp_2}{dx} [C_1 \cosh Ny + C_2 \sinh Ny - 1] \\
 & + \frac{\varepsilon(1 + \lambda_1)}{2N^2} \frac{dp_1}{dx} \left[\frac{\sinh Ny(h_1 \cosh Nh_2 - h_2 \cosh Nh_1)}{\sinh N(h_1 - h_2)} - 2y \right. \\
 & \quad + C_1 y \cosh Ny + C_2 y \sinh Ny \\
 & \quad \left. + \frac{\cosh Ny(h_2 \sinh Nh_1 - h_1 \sinh Nh_2)}{\sinh N(h_1 - h_2)} \right] \\
 & + \frac{dp_0}{dx} \frac{\varepsilon(1 + \lambda_1)}{4N^2} \left[\frac{C_1(y \sinh Ny + Ny^2 \cosh Ny) + C_2(y \cosh Ny + y^2 N \sinh Ny)}{2N} \right. \\
 & \quad - y^2 + \frac{(1 - \cosh N(h_1 - h_2))(\sinh Ny(h_1 \cosh Nh_2 + h_2 \cosh Nh_1))}{2\sinh^2 N(h_1 - h_2)} \\
 & \quad - \frac{(1 - \cosh N(h_1 - h_2))((h_1 \sinh Nh_2 + h_2 \sinh Nh_1) \cosh Ny)}{2\sinh^2 N(h_1 - h_2)} \\
 & \quad - \frac{(h_1 \cosh Nh_2 - h_2 \cosh Nh_1)(C_1 y \cosh Ny + C_2 y \sinh Ny)}{(\cosh Nh_1 - \cosh Nh_2)} \\
 & \quad \left. + \frac{(h_2^2 \cosh Nh_1 - h_1^2 \cosh Nh_2) \sinh Ny}{2 \sinh N(h_1 - h_2)} \right]
 \end{aligned}$$

$$\begin{aligned}
& + \frac{(h_1^2 \sinh Nh_1 - h_2^2 \sinh Nh_2) \cosh Ny}{2 \sinh N(h_1 - h_2)} \\
& \times \left. \frac{8(1 - C_1 \cosh Ny - C_2 \sinh Ny)}{N^2} + \frac{(h_1 - h_2)y \cosh Ny}{(\cosh Nh_1 - \cosh Nh_2)} \right], \quad (3.18)
\end{aligned}$$

and the volume flow rate q_2 is given by

$$q_2 = \int_{h_2}^{h_1} u_2 dy. \quad (3.19)$$

From (3.18), we have

$$\begin{aligned}
\frac{dp_2}{dx} = & Aq_2 + \frac{A\varepsilon(1 + \lambda_1)}{2N^3} \frac{dp_1}{dx} \left[\frac{2(h_1 + h_2)(1 - \cosh N(h_1 - h_2))}{\sinh N(h_1 - h_2)} + N((h_1^2 - h_2^2)) \right] \\
& - \frac{A\varepsilon(1 + \lambda_1)}{4N^3} \frac{dp_0}{dx} \left[\frac{8(h_1 - h_2)}{N} - \frac{3(h_1 - h_2)}{2N} - \left(\frac{h_1^3}{3} - \frac{h_2^3}{3} \right) \right] \\
& + \frac{(h_1^2 + h_2^2)(1 - \cosh N(h_1 - h_2))}{2N \sinh N(h_1 - h_2)} + \frac{(h_1 - h_2)(h_1 \sin Nh_1 - h_2 \sin Nh_2)}{(\cosh Nh_1 - \cosh Nh_2)} \\
& + \frac{(h_1 + h_2)(1 - \cosh N(h_1 - h_2))(h_1 \cosh Nh_2 - h_2 \cosh Nh_1)}{\sinh N(h_1 - h_2)(\cosh Nh_1 - \cosh Nh_2)} \\
& + \frac{(h_1^2 N^2 + h_2^2 N^2 + 2)(\cosh N(h_1 - h_2) - 1)}{2N^2 \sinh N(h_1 - h_2)} + \frac{16(1 - \cosh N(h_1 - h_2))}{N^2 \sinh N(h_1 - h_2)}. \quad (3.20)
\end{aligned}$$

The dimensionless pressure rise at this order is

$$\Delta P_2 = \int_0^2 \frac{dp_2}{dx} dx. \quad (3.21)$$

Summarizing the result obtained from (3.11), (3.16), and (3.20), we write

$$\Delta P = \Delta P_0 + \alpha \Delta P_1 + \alpha^2 \Delta P_2. \quad (3.22)$$

Corresponding stream functions can be defined as

$$u = \frac{\partial \Psi}{\partial y}, \quad v = -\delta \frac{\partial \Psi}{\partial x}. \quad (3.23)$$

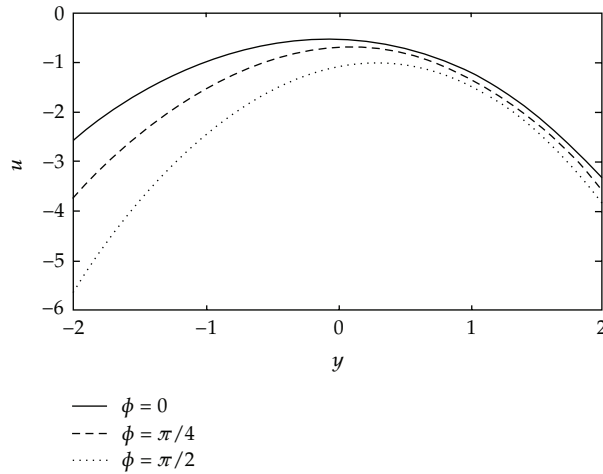


Figure 10: Axial velocity versus y at $\alpha = 0.05$, $a = 0.2$, $b = 0.6$, $d = 0.8$, $\varepsilon = 0.2$, $\lambda_1 = 1$, $Da = 1$, $x = \pi/2$, and $q = -1$.

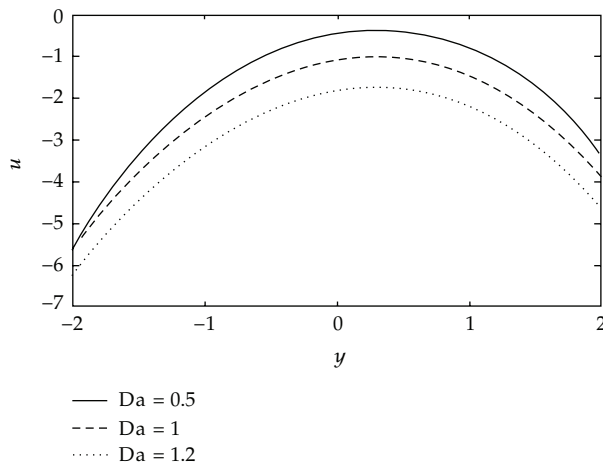


Figure 11: Axial velocity versus y at $\alpha = 0.05$, $a = 0.2$, $b = 0.6$, $d = 0.8$, $\varepsilon = 0.2$, $\lambda_1 = 1$, $q = -1$, $x = \pi/6$, and $\phi = \pi/2$.

4. Results and Discussion

We have used a regular perturbation series in term of the dimensional viscosity parameter α to obtain analytical solution of the field equations for peristaltic flow of Jeffrey fluid in an asymmetric channel. To study the behavior of solutions, numerical calculations for several values of viscosity parameter α , Daray number Da , porosity ε , amplitude ratio ϕ , Jeffrey fluid parameter λ_1 , a and b have been calculated numerically using MATHEMATICA software.

Figure 1 shows the variation of ΔP with flow rate θ for different values of α . It is depicted that the time-average flux θ increase with increasing the viscosity parameter α . Figure 2 represents the variation of ΔP with the flow rate θ for different values of Da . We observe that an increase in the peristaltic pumping rate pressure rises. Figures 3 and 4 are graphs of pressure rise ΔP with the flow rate θ for values of ε and λ_1 . It is observed that the

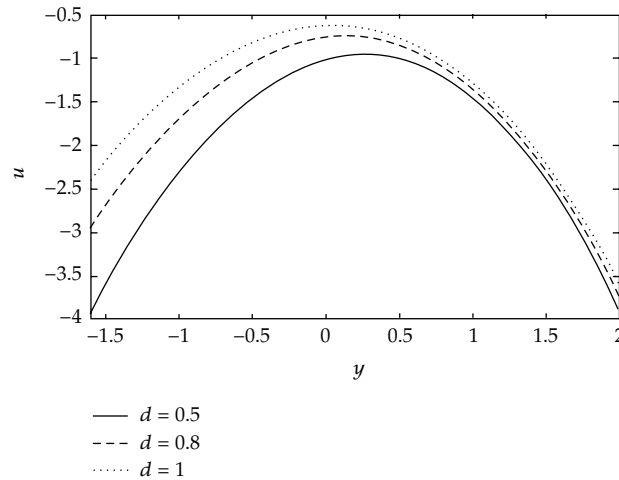


Figure 12: Axial velocity versus y at $\alpha = 0.05$, $a = 0.2$, $b = 0.6$, $q = -1$, $\varepsilon = 0.2$, $\lambda_1 = 1$, $Da = 1$, $x = \pi/6$, and $\phi = \pi/2$.

pumping rate decreases with increase of ε and λ_1 . Figure 5 is the graph of the variation of ΔP versus the flow rate θ for different values of phase difference ϕ . It is observed that the pumping rate decreases with the increase of ϕ . Figures 6 and 7 plot the relation between pressure rise ΔP and flow rate θ for different values of a and b , respectively. Figure 8 represents the graph of axial velocity u versus y . It can be seen that an increase in α decreases the magnitude of axial velocity u . The effects of q on the axial velocity u are seen through Figure 9. It is noticed that an increase in q increase the magnitude of the axial velocity. Figures 10 and 11 illustrate the effect of phase difference ϕ and Daray's number Da on the axial velocity u . It is observed that the magnitude of axial velocity decreases with the increasing phase difference ϕ and Daray's number Da . In Figure 12 the axial velocity u is graphed versus y . We note that the magnitude of axial velocity increases as the channel width d increases. It is worth mentioning that in the absence of porosity parameter the solutions of [10] can be derived as special case of the present analysis. This provides the useful check. It may be remarked that the problem for this particular model was not solved earlier even by any traditional perturbation technique. The results presented in this paper will now be available for experimental verification.

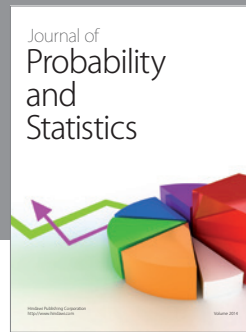
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